

Investigation of Sampling
Geometry for Simultaneous
Emissions / Immunity
Calibration of Free Space
Chambers

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Overview

- History : What's wrong with Normalized Site Attenuation Criteria of ± 4 dB ?
- Background : Proposed Method of Simultaneous Emissions/Immunity Calibration in Free Space Chambers
- Calibration Geometry : Uniform Plane vs. Volumetric Sampling
- Experimental Results for a typical chamber
- Conclusions

Radiated Emissions Model

Emissions Source
(dBuV/m)



+Ideal Site Attenuation (dB)



+Non-Ideal Site Attenuation
(+/- 4 dB to Ideal)



+Other Transducers
(antenna, cables, pre-amp, +/- dB)

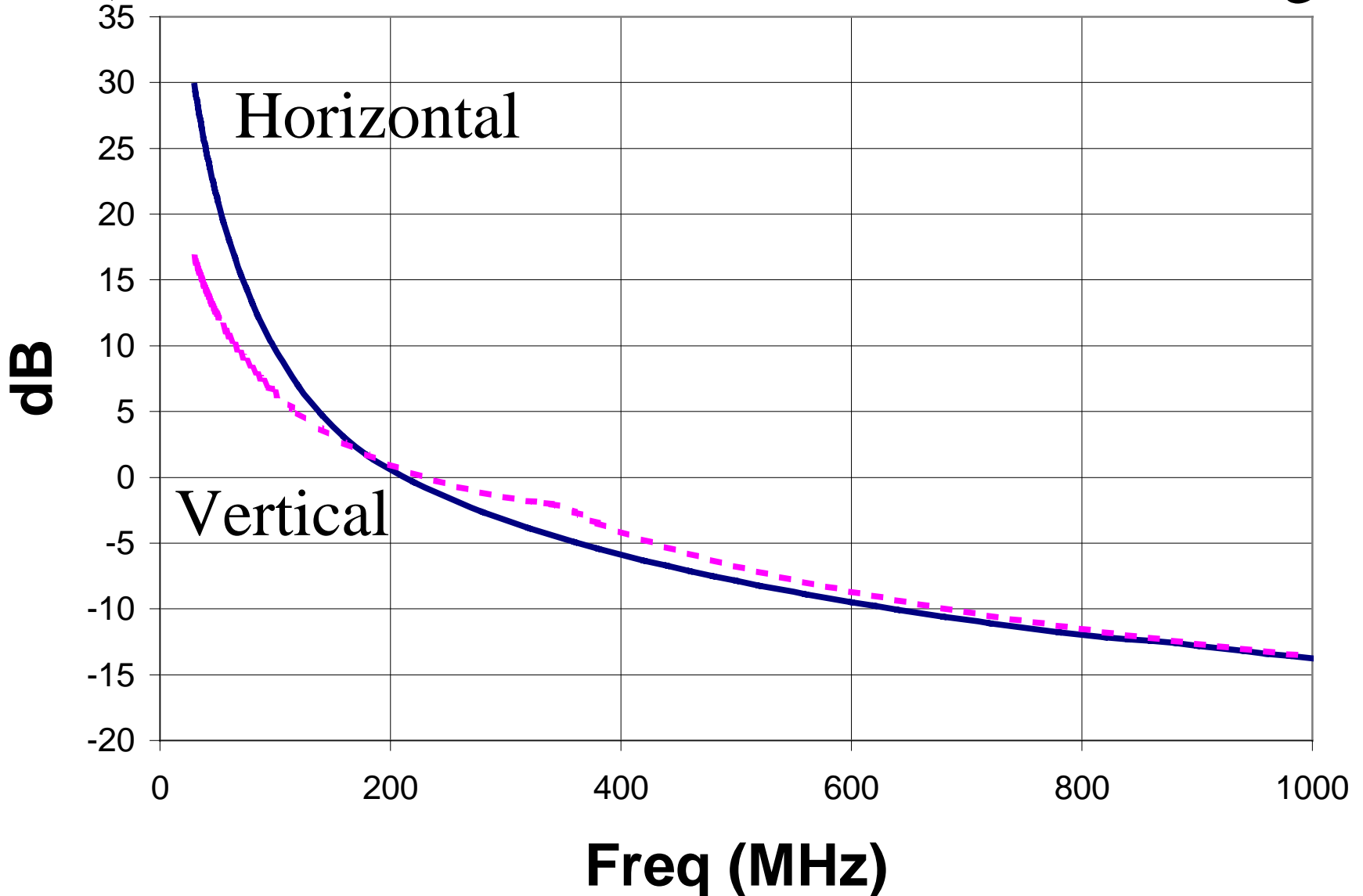


Measurement (dBuV/m)

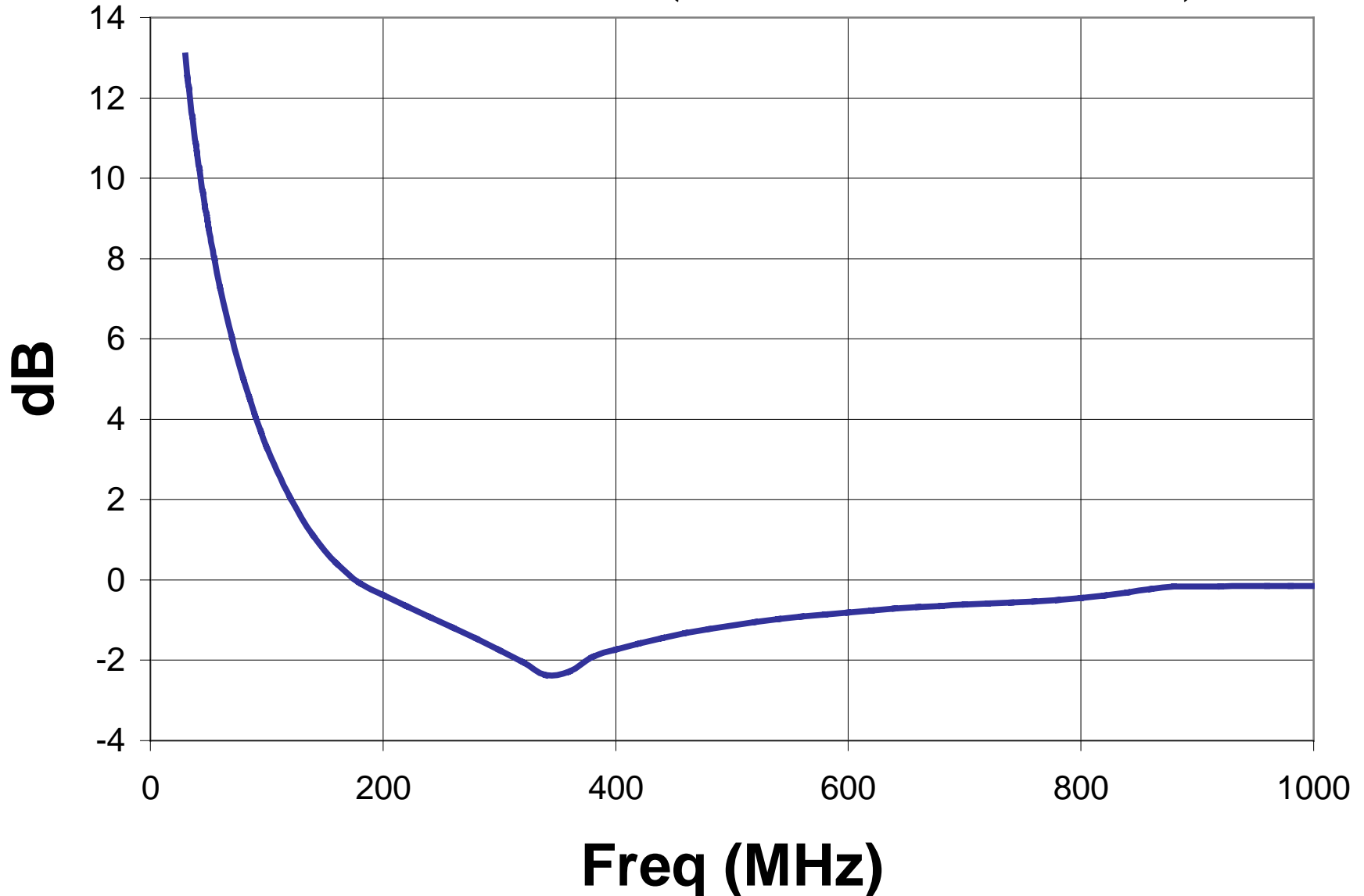
→ Compare to
Limit

Ideal 10m OATS Site Attenuation

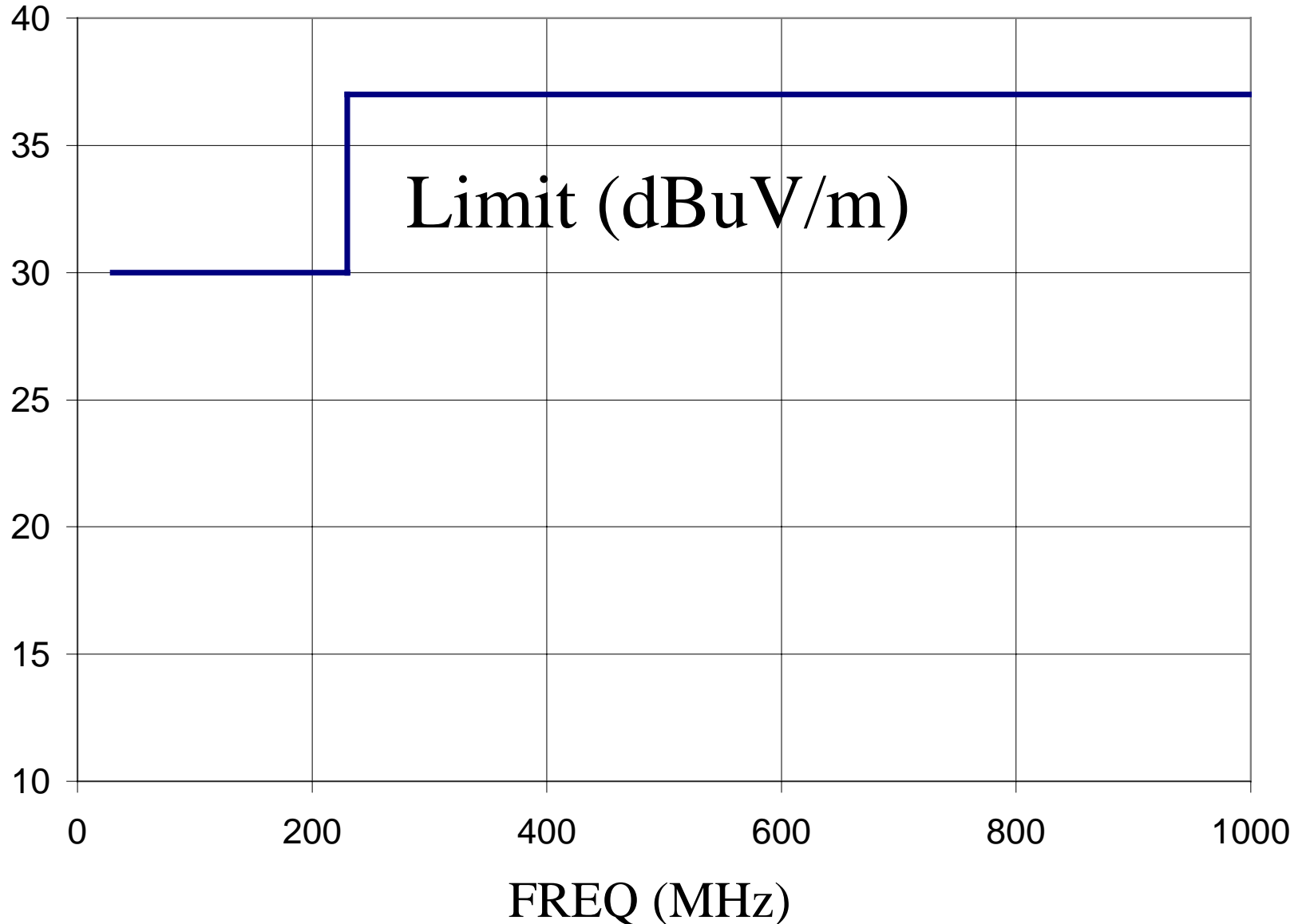
(source ANSI C63.4, Table 1, 1m source height)



Difference In Ideal 10m OATS Site Attenuation (Horiz/Vert, dB)



CISPR 22 Specification Limit (dBuV/m at 10 meters, Horiz or Vert)



Site Attenuation on OATS : What's Wrong?

- The IDEAL 10m OATS site attenuation produces large differences in actual measurements (H vs. V) even for the very basic example of a 1 meter source height above ground.
- But Limits for Horiz or Vert are the same!
- Application of Limits is not the same due to the IDEAL characteristics of the chosen model test facility (the OATS).
- Problem is even worse when different source locations are considered.

Why Free Space?

- Free space methods solve the inconsistencies in the IDEAL site model : Ideal Site Attenuation is the same regardless of polarity and independent of emissions source location in the test volume.
- Why not just use Free Space NSA of +/-4 dB to ideal for validation of free space chambers? (McConnell and Vitek, IEEE 1996 EMC Symposium, also prEN50147 part 3)

Free Space NSA Validation?

- Deviation from Ideal NSA (ΔNSA) is required to be within ± 4 dB to ideal model.
- Consider NSA results for the following two sites :
 - Site 1 : All positions = $+4$ dB ± 0.2 dB
 - Site 2 : All positions = -4 dB ± 0.2 dB
- Thus, 8 dB Error still exists in Site to Site Measurements between validated sites!

Problems with NSA +/- 4 dB methods

- Deviation from ideal NSA (Δ NSA) is an error term not an uncertainty. Error terms require determination and compensation in subsequent measurements.
- The Type A uncertainty component (the +/- 0.2 dB in this example) is presently unused.
- Result: NSA validation methods are not consistent with *NIST Technical Note 1297* or ISO Guide for expression of Uncertainty in Measurement (ISO GUM).

Simultaneous Emissions/Immunity Calibration of Free Space Chambers

- Key Proposal :
 - Use a single procedure to simultaneously calibrate facility, antenna, and cabling for emissions and immunity.
 - Results traceable to National Reference (NIST) through reference instrumentation : error and uncertainty calculated in accordance with ISO guide.

Simultaneous Emissions/Immunity Calibration of Free Space Chambers

- Requirements
 - Must use single facility (Free Space Chamber) and equipment set (antenna, cables) as a system.
 - Must harmonize the calibration geometry (plane vs. volume) to enable a single procedure to be used.

Simultaneous Emissions/Immunity Calibration of Free Space Chambers

- Relationship between NSA (emissions) and IEC 61000-4-3 (immunity) Calibration :

$$NSA = \frac{V_{direct}}{V_{site}} \cdot \frac{1}{AF_1} \cdot \frac{1}{AF_2}$$

$$V_{direct} = \sqrt{P_F \cdot R_L}$$

Simultaneous Emissions/Immunity Calibration of Free Space Chambers

And,

$$V_{site} = \frac{E}{AF_2}$$

Substitute for V_{direct} and V_{site} :

$$NSA = \frac{\sqrt{P_F \cdot R_L}}{\frac{E}{AF_2}} \cdot \frac{1}{AF_1} \cdot \frac{1}{AF_2}$$

Simultaneous Emissions/Immunity Calibration of Free Space Chambers

If ideal NSA is used as the reference, no previous AF's are needed (AF_1 is determined by measurement of E and P_F).

$$AF_1 = \frac{\sqrt{50 \cdot P_F}}{E \cdot NSA_{Ideal}}$$

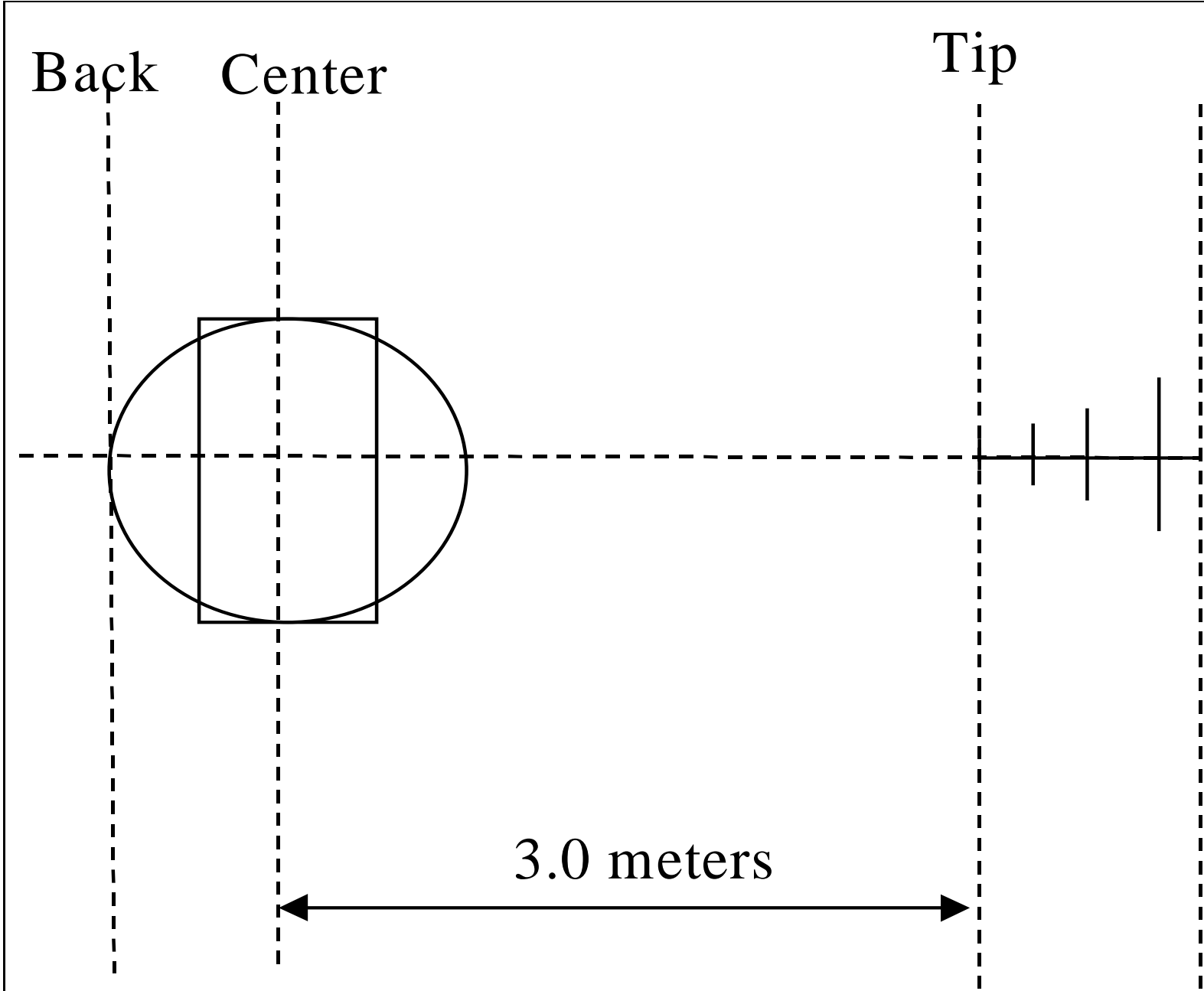
Simultaneous Emissions/Immunity Calibration of Free Space Chambers

- When measured values of E and P_F are used, AF_1 will include full transducer error of antenna, facility and cables.
- Problem? No. This is exactly what we want (the error term for the system).
- Rename AF_1 the “combined correction factor”, in dB = C_{dB} to clearly indicate a system combined factor, not just an antenna factor anymore.

Simultaneous Emissions/Immunity Calibration of Free Space Chambers

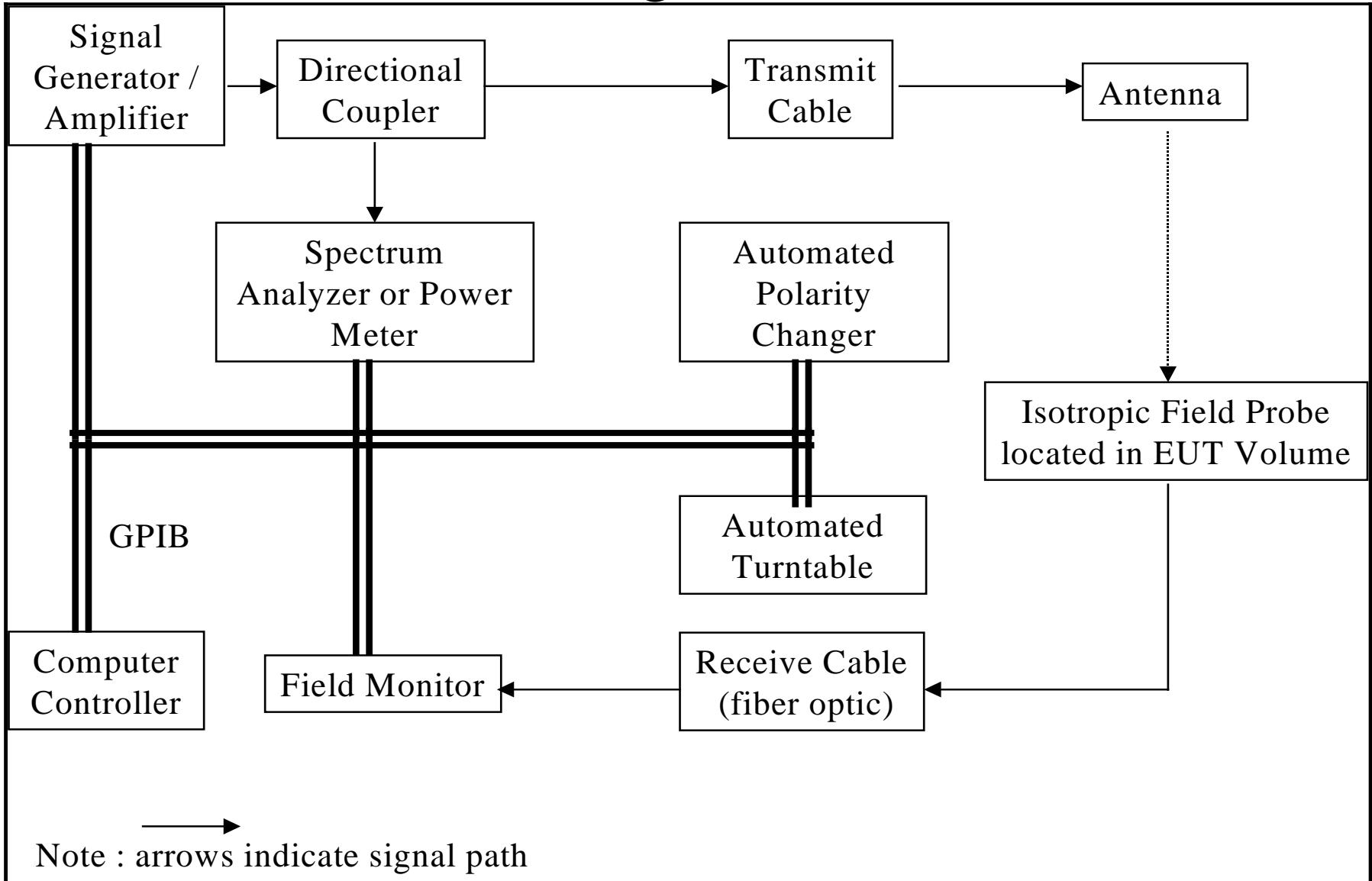
- Preceding is valid for a single point.
What about sampling over a plane or a volume?
- Proposal : compute average C_{dB} and uncertainty from a population of sample points.
- Use a Plane similar to IEC61000-4-3 or a volume similar to ANSI C63.4?

Simultaneous
Emissions/Immunity
Calibration
Procedure

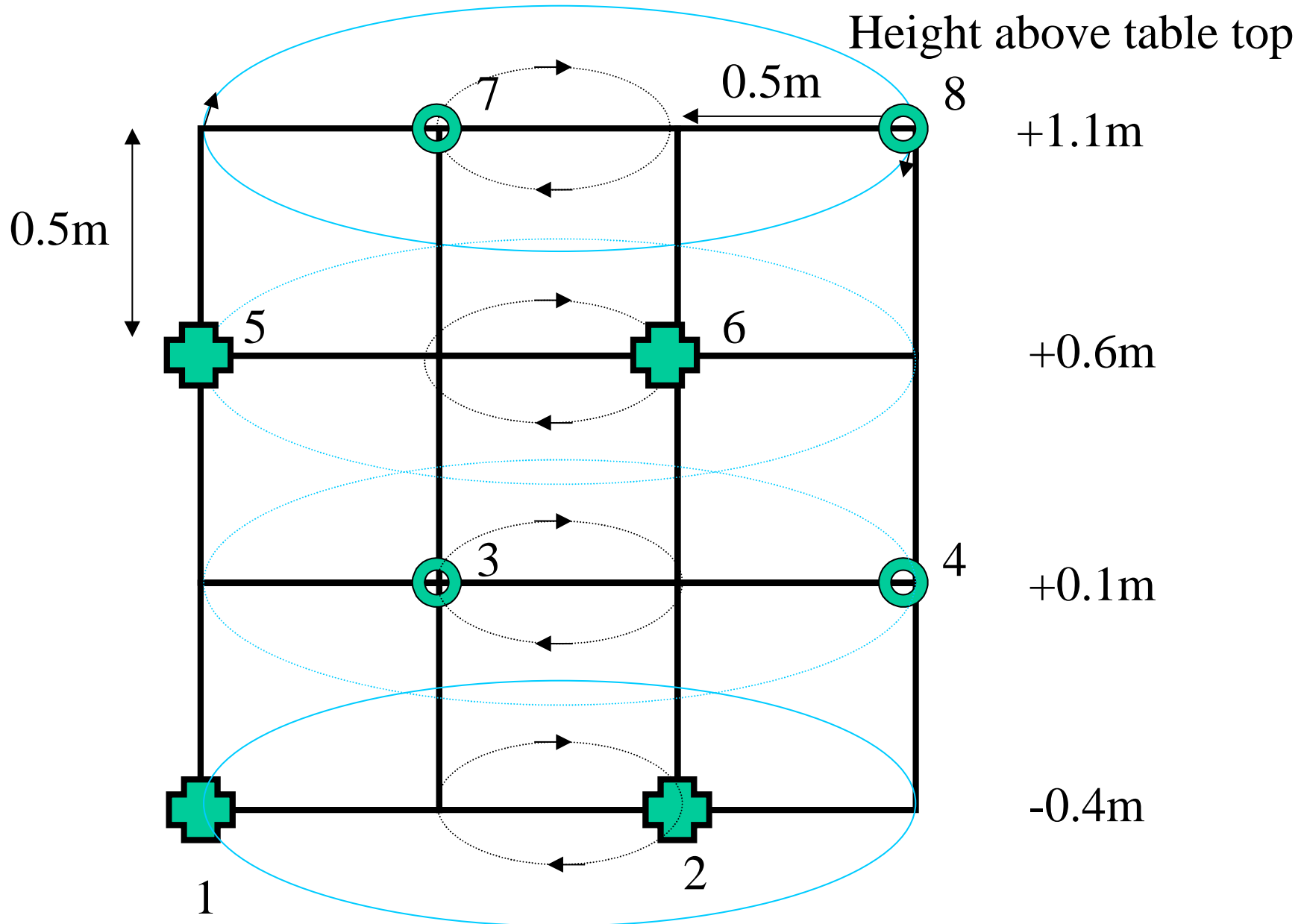


CALIBRATION PROCEDURE

(Figure 1)



SAMPLING GEOMETRY (FIGURE 2)



RESULTS FOR A TYPICAL CHAMBER

Plane vs. Volume

- System Gain
- System Transducer (CdB)
- Uncertainty over Plane or Volume

Multiple Samples

See Symposium Record (SR), Equations 1 - 5 :

Average Forward Power (normalized to 1 V/m)

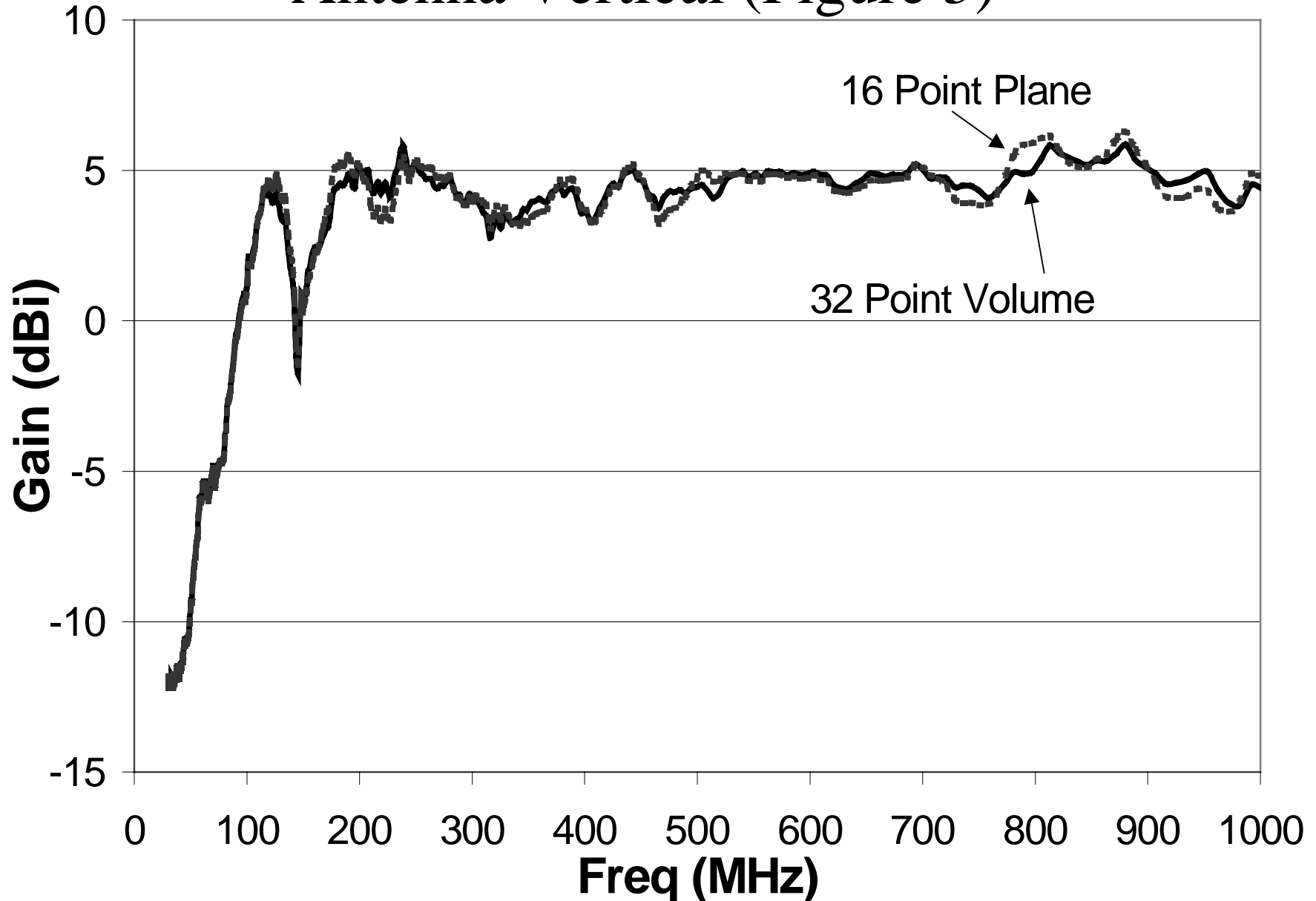
$$\overline{P_f}(\text{watts}) = \sum_{i=1}^n \frac{P_{f_i}(\text{watts})}{n} \quad (1)$$

Average System Gain over isotropic :

$$\overline{G}_{dBi} = 10 \cdot \log \left(\frac{E^2 \cdot d^2}{30 \cdot \overline{P_F}} \right) \quad (4)$$

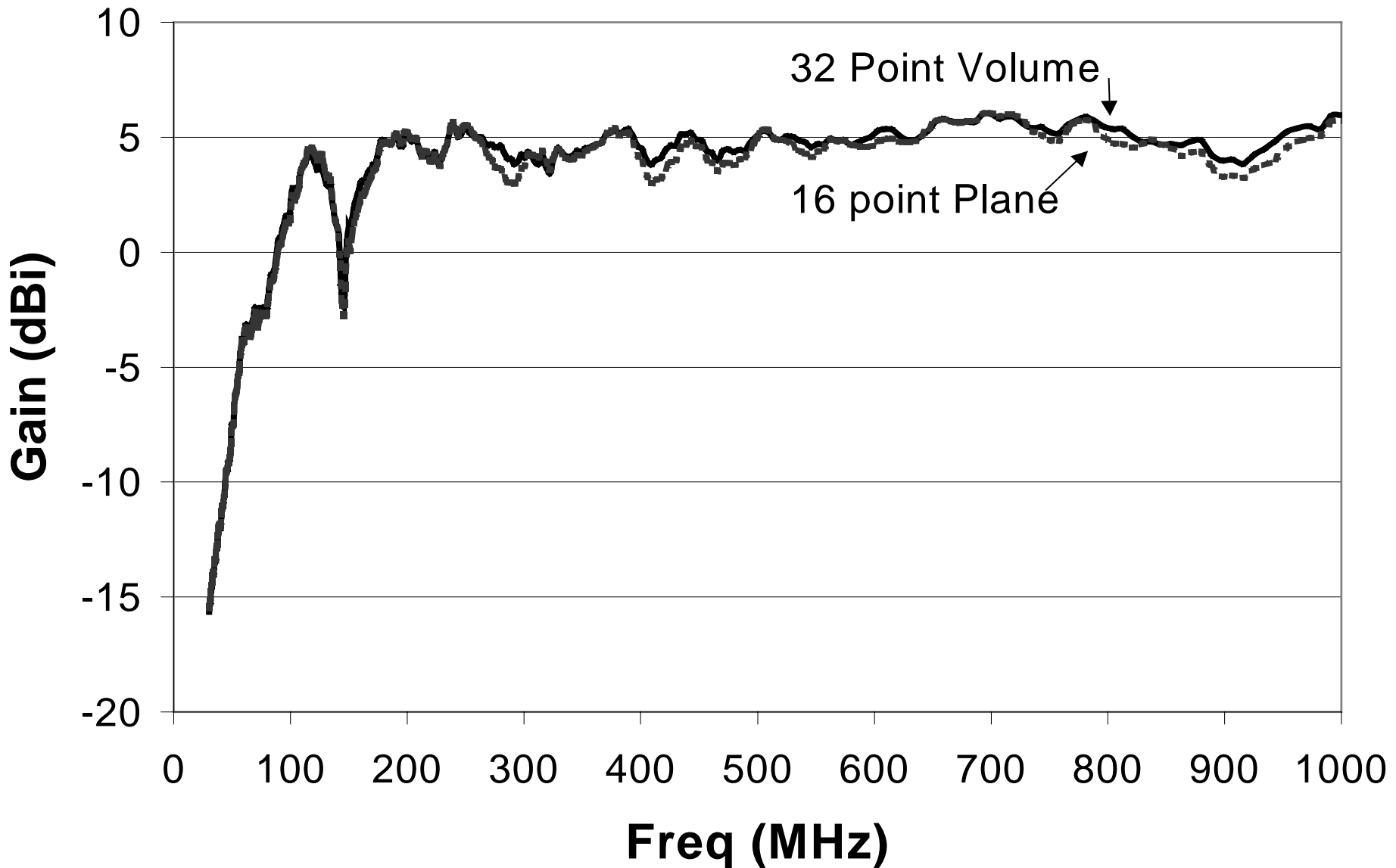
RESULTS FOR A TYPICAL CHAMBER : GAIN

Antenna Vertical (Figure 5)



RESULTS FOR A TYPICAL CHAMBER : GAIN

Antenna Horizontal (Figure 6)



Average System Transducer Factor (C_{dB}) :
(computed from Gain, in decibels)

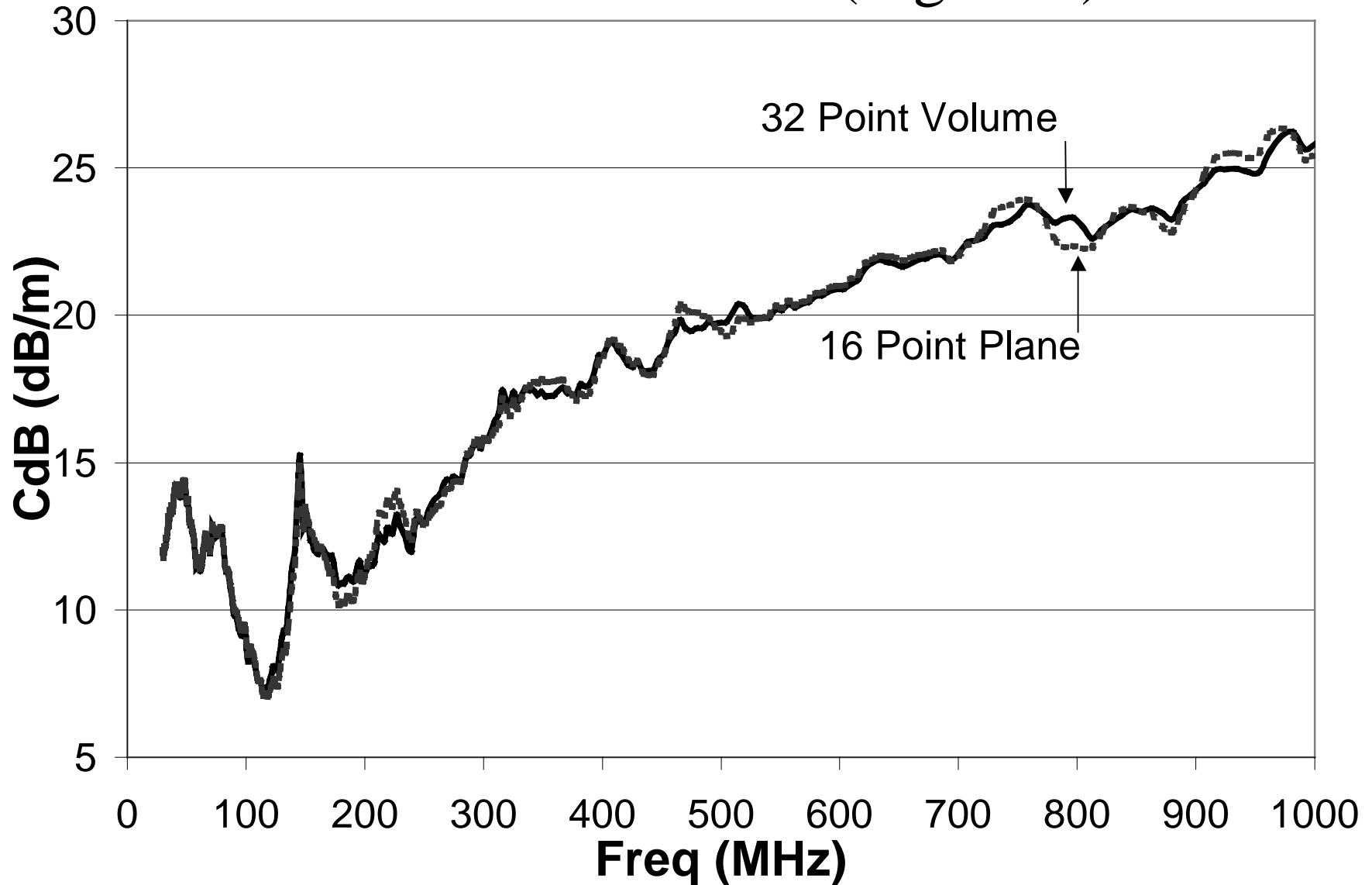
$$\overline{C}_{dB} = 20 \cdot \log(f_{MHz}) - 29.77 - \overline{G}_{dBi} \quad (5)$$

Or, as shown before C_{dB} can also be written in terms of ideal NSA :

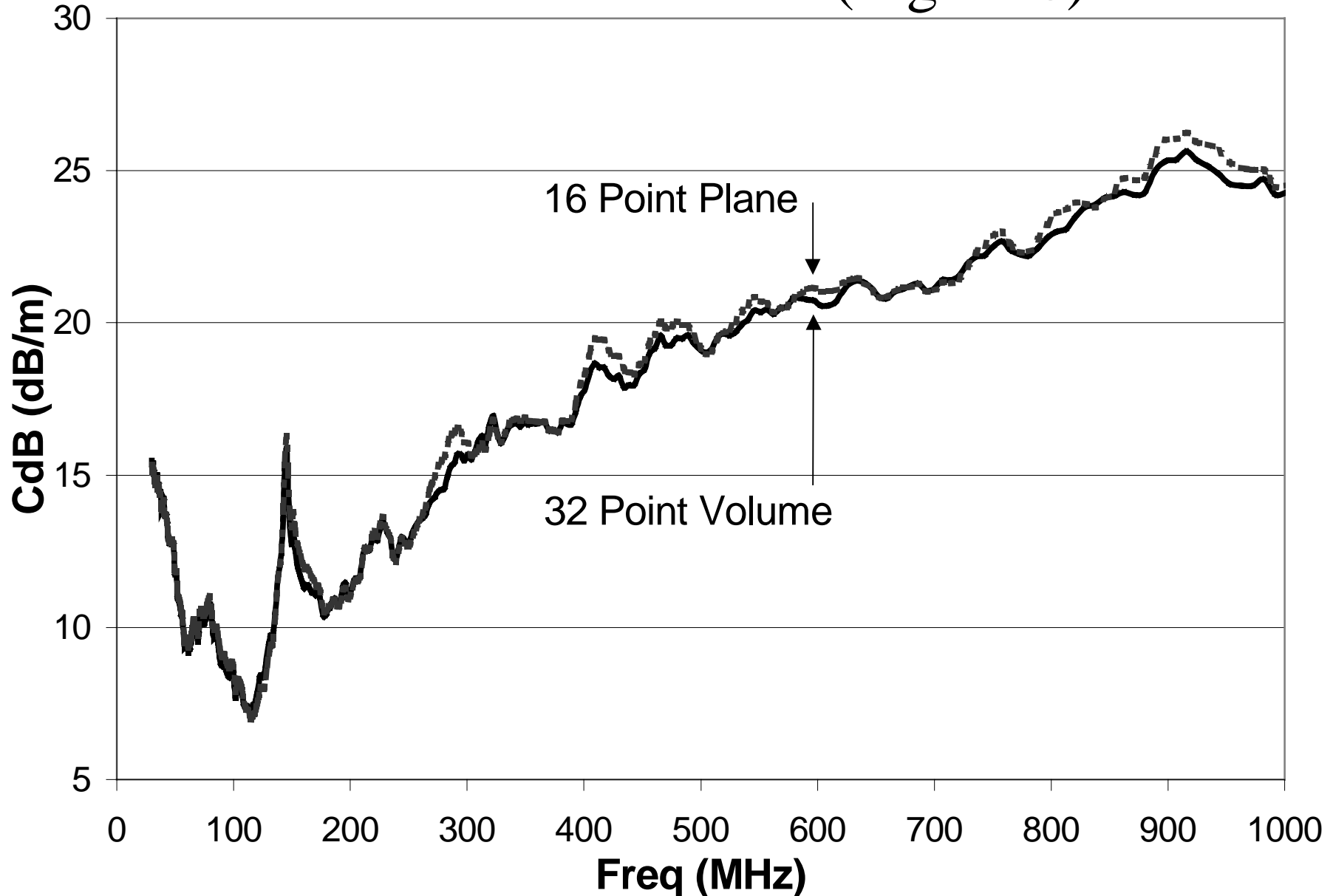
$$\overline{C}_{dB} = 20 \cdot \log\left(\frac{\sqrt{50 \cdot \overline{P}_F}}{E \cdot NSA_{Ideal}}\right)$$

RESULTS FOR A TYPICAL CHAMBER : C_{dB}

Antenna Vertical (Figure 7)



RESULTS FOR A TYPICAL CHAMBER : C_{dB} Antenna Horizontal (Figure 8)

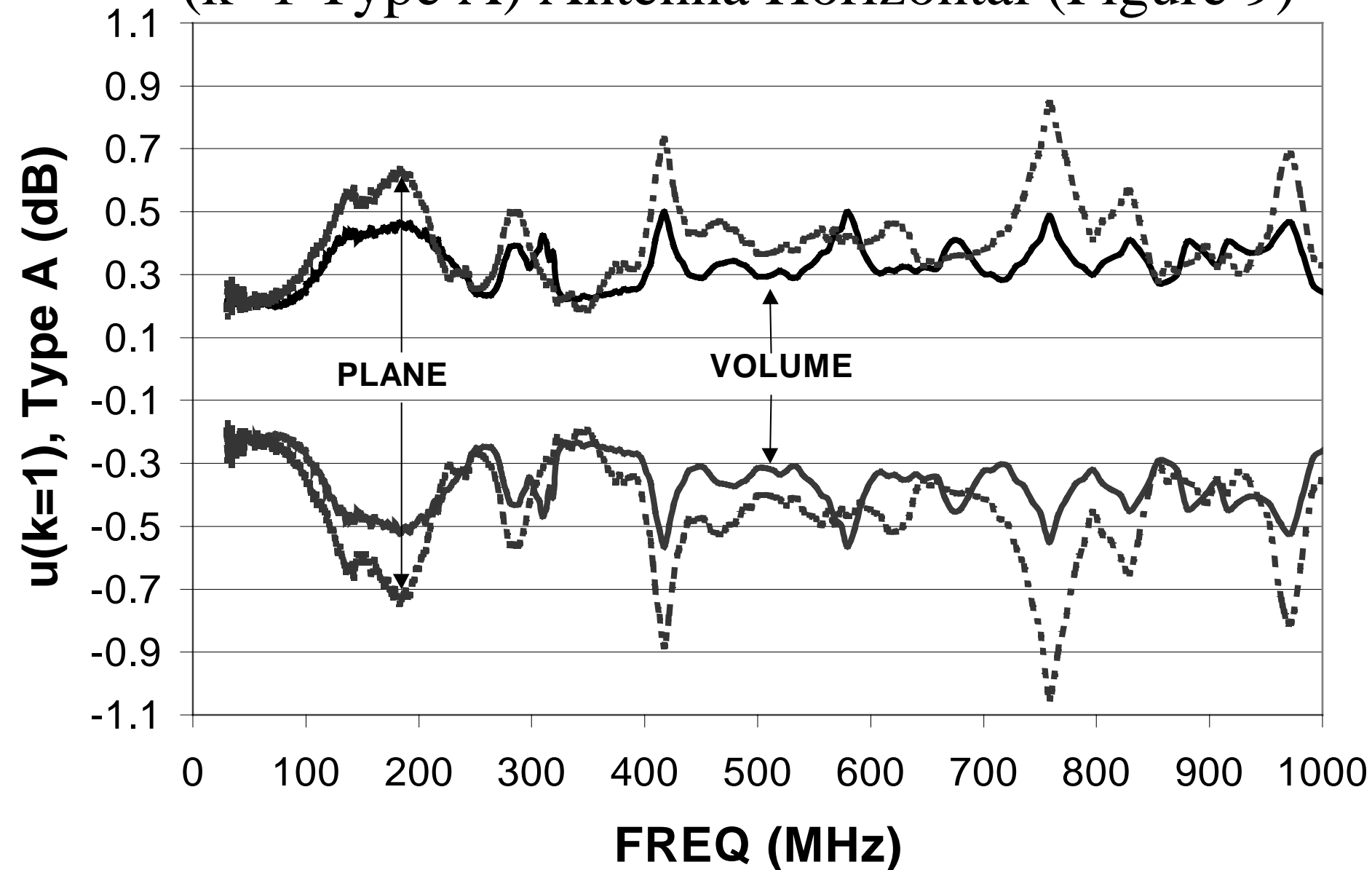


Standard Deviation and Uncertainty in Average Values (example : P_F)

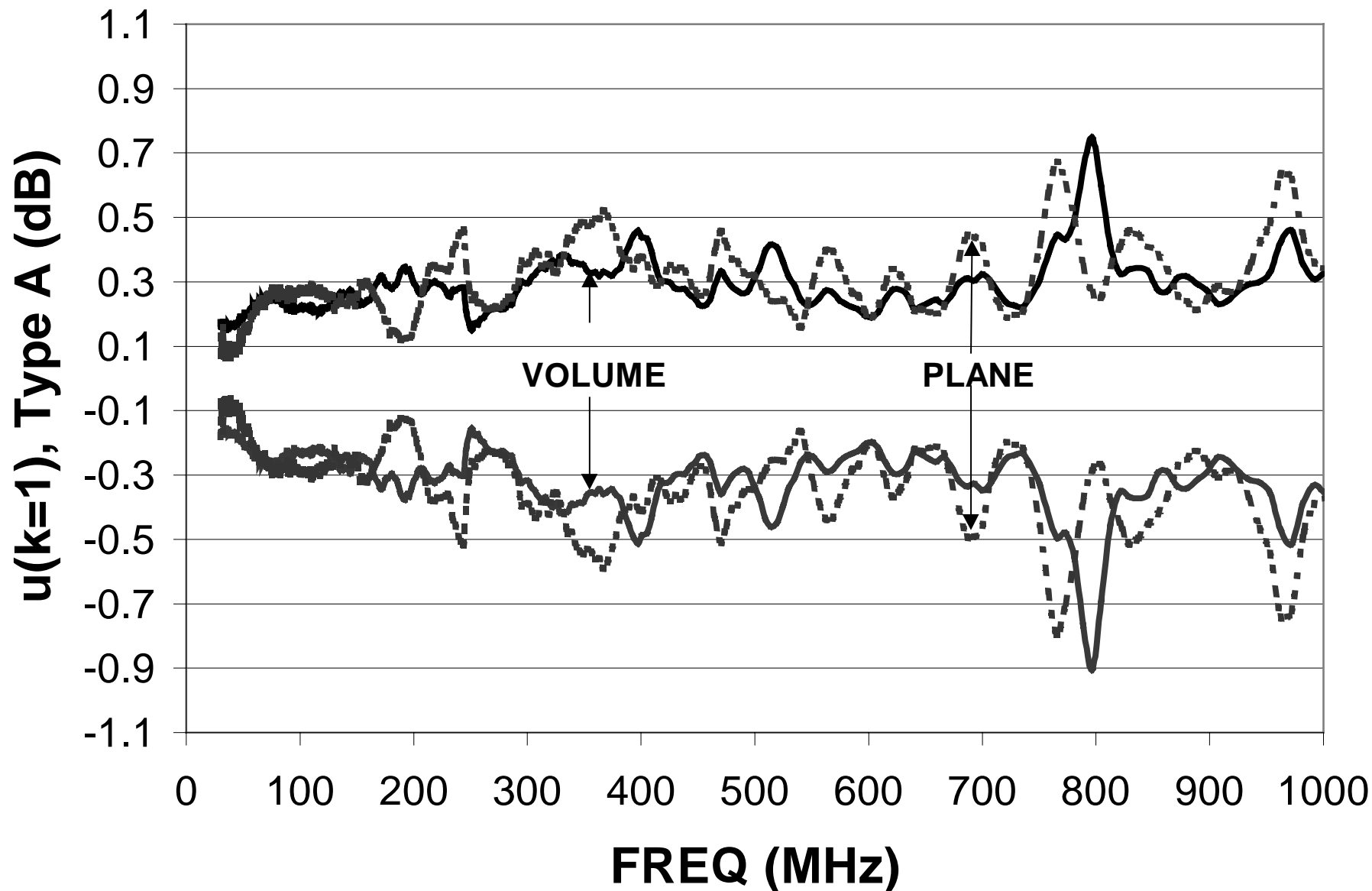
$$s = \sqrt{\frac{n \cdot \sum_{i=1}^n P_{f_i}^2 - \left(\sum_{i=1}^n P_{f_i} \right)^2}{n \cdot (n-1)}} \quad (2)$$

$$u = \frac{s}{\sqrt{n}} \quad (3)$$

Uncertainty Results for Typical Chamber : u_{dB} ($k=1$ Type A) Antenna Horizontal (Figure 9)



Uncertainty Results for Typical Chamber : u_{dB} (k=1 Type A) Antenna Vertical (Figure 10)



Total, combined expanded uncertainty of instrumentation and facility is Root Sum Squares (RSS) combined Type A and Type B uncertainties (equation 6):

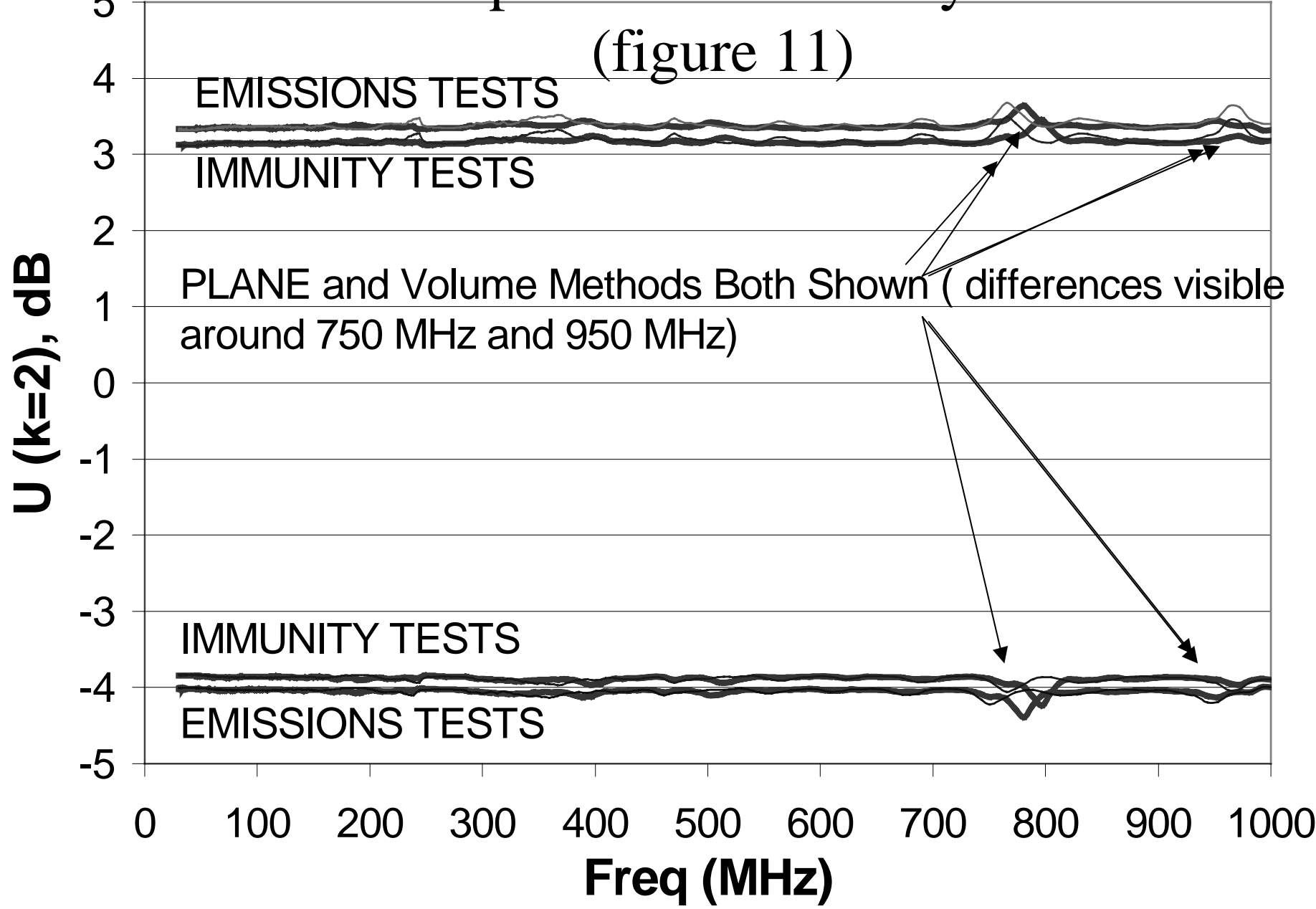
$$U = 2 \cdot \sqrt{u_{probe}^2 + u_{dircoupler}^2 + u_{meter}^2 + u_{preamp}^2 + u_{typeA}^2}$$

Uncertainty : Type B (instrumentation) Factors (Table 1)

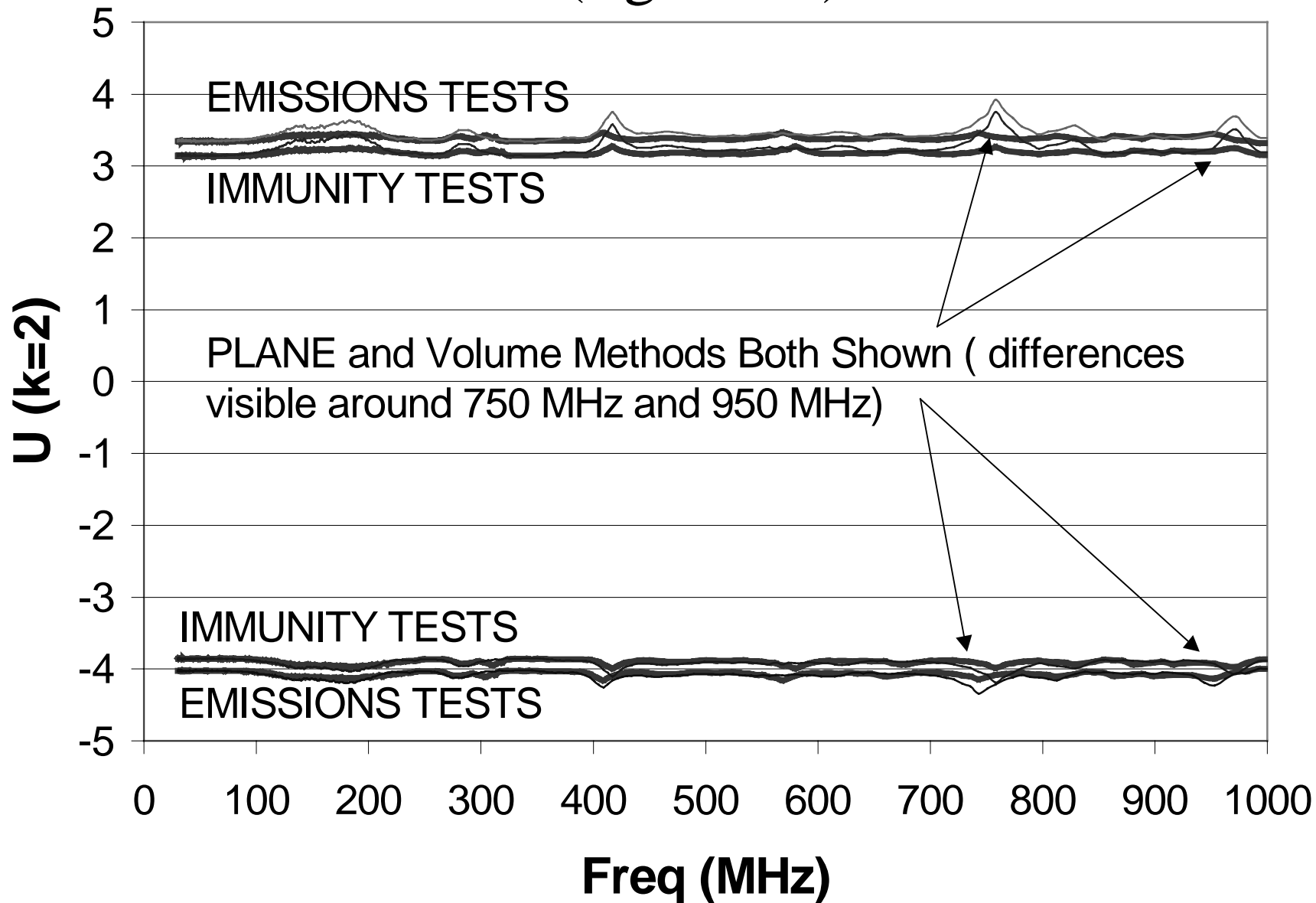
Device	Type	Standard Value (k=1)
Field Probe	Normal(k=2)	+1/-1.5 dB
Meter	Rectangular(k=1.73)	+/- 1.15 dB
Dir. Coupler	Rectangular(k=1.73)	+/-0.289 dB
Pre-Amplifier	Rectangular(k=1.73)	+/-0.577 dB

Combined Expanded Uncertainty : Horizontal

(figure 11)



Combined Expanded Uncertainty : Vertical (figure 12)



CONCLUSIONS

- Proposed procedure provides NIST traceable (and ISO Guide compliant) error and uncertainty information not possible with NSA methods.
- A single, harmonized calibration procedure could be used for a free space chamber for emissions and immunity tests.
- Proposed procedure provides simultaneous calibration of chamber, antenna, and cables.

Conclusions

- PLANE vs. Volume? Little real difference (<0.6 dB) observed in error and uncertainty terms for typical free space chamber.
- Proposal : Just use a 16 point plane sampling geometry for up to 1.5m diameter test volume. Results valid for emissions and immunity chamber validation.

Acknowledgements

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